

**Granular Explosives
and Initiation Sensitivity**

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Outline

- Explosives
 - Homogeneous (premixed gas)
 - Thermal explosion theory
 - Heterogeneous (Plastic Bonded Explosive)
 - Temperature fluctuations
 - Temperature sensitive reaction rate
- Shock initiation
 - Experimental phenomena
- Homogenized reactive models
 - Fluctuations not resolved
 - Phenomenological burn models
 - Account for sub-grid physics
 - Assumptions limit domain of applicability
- Granular explosives
 - Model for damaged explosives
 - More sensitive
 - Exacerbates effect of hot spots (Bowden-Yoffe)
- ▶ **Meso-Mechanics Simulations**
 - Compaction Waves in Granular bed
 - Subgrain fluctuations
 - Temperature distribution
- ▶ **Improved Sub-grid Burn Models**
 - Physics issues

Shock-to-Detonation Transition

Homogeneous explosive

(Campbell, Davis & Travis)

1. Thermal runaway at piston leads to detonation.
2. Detonation wave overtakes lead shock.
3. Detonation speed slows until CJ wave is formed.

Heterogeneous explosive

(Campbell, Davis, Ramsay & Travis)

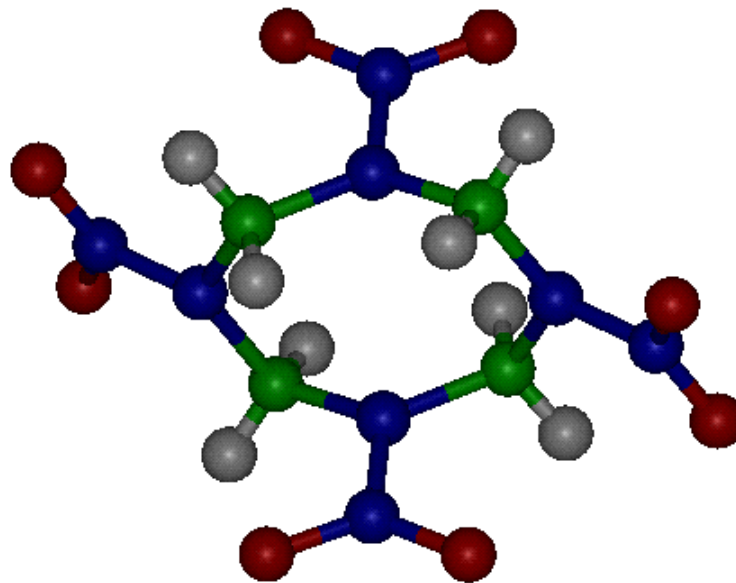
1. The lead wave is a reactive shock.
2. Abrupt transition to detonation ahead of piston.
3. No overshoot in detonation speed
Explosive next to piston only partially burned.

Qualitatively different behavior

Wedge experiments

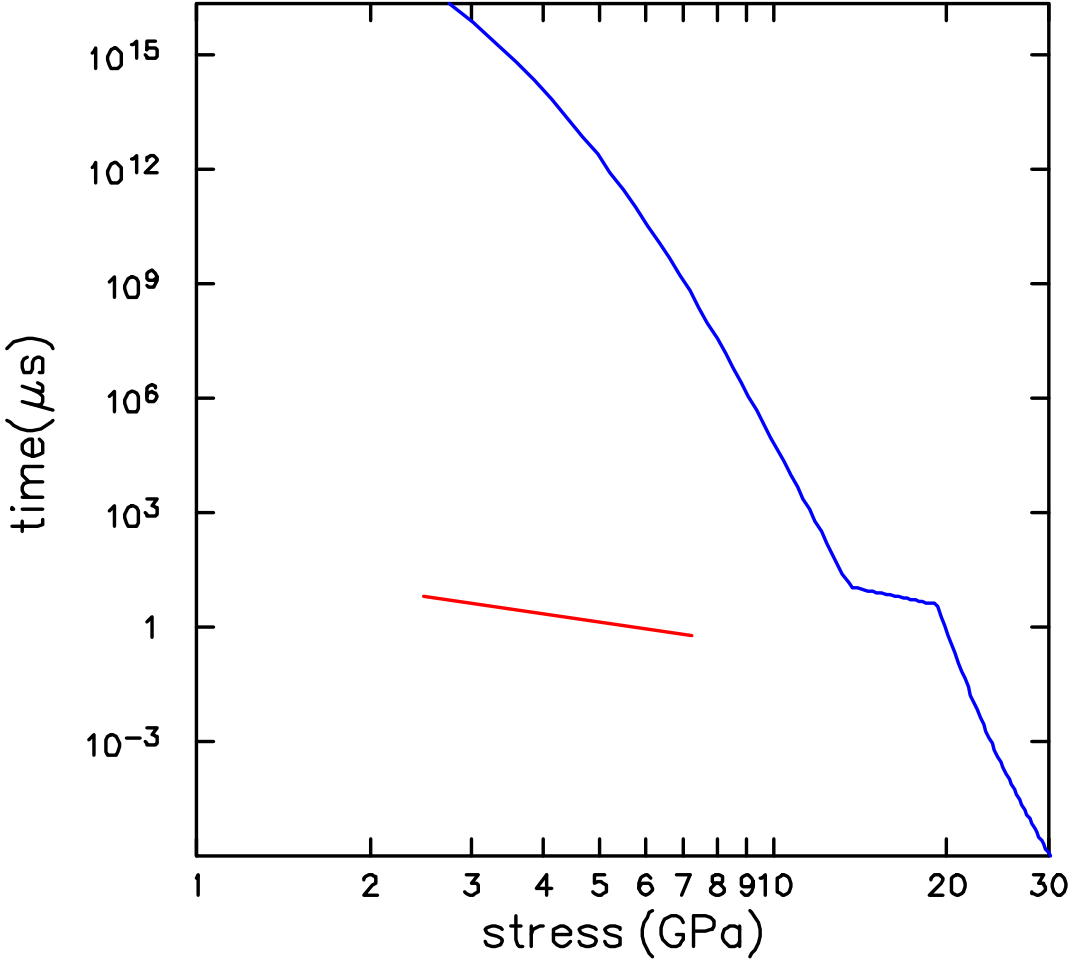
1. Measure shock trajectory
2. Pop-plot
Distance of run vs. shock pressure
Linear on log-log plot over range of experiments

Examples for HMX
(cyclo-tetramethylene-tetranitramine, $C_4H_8N_8O_8$)



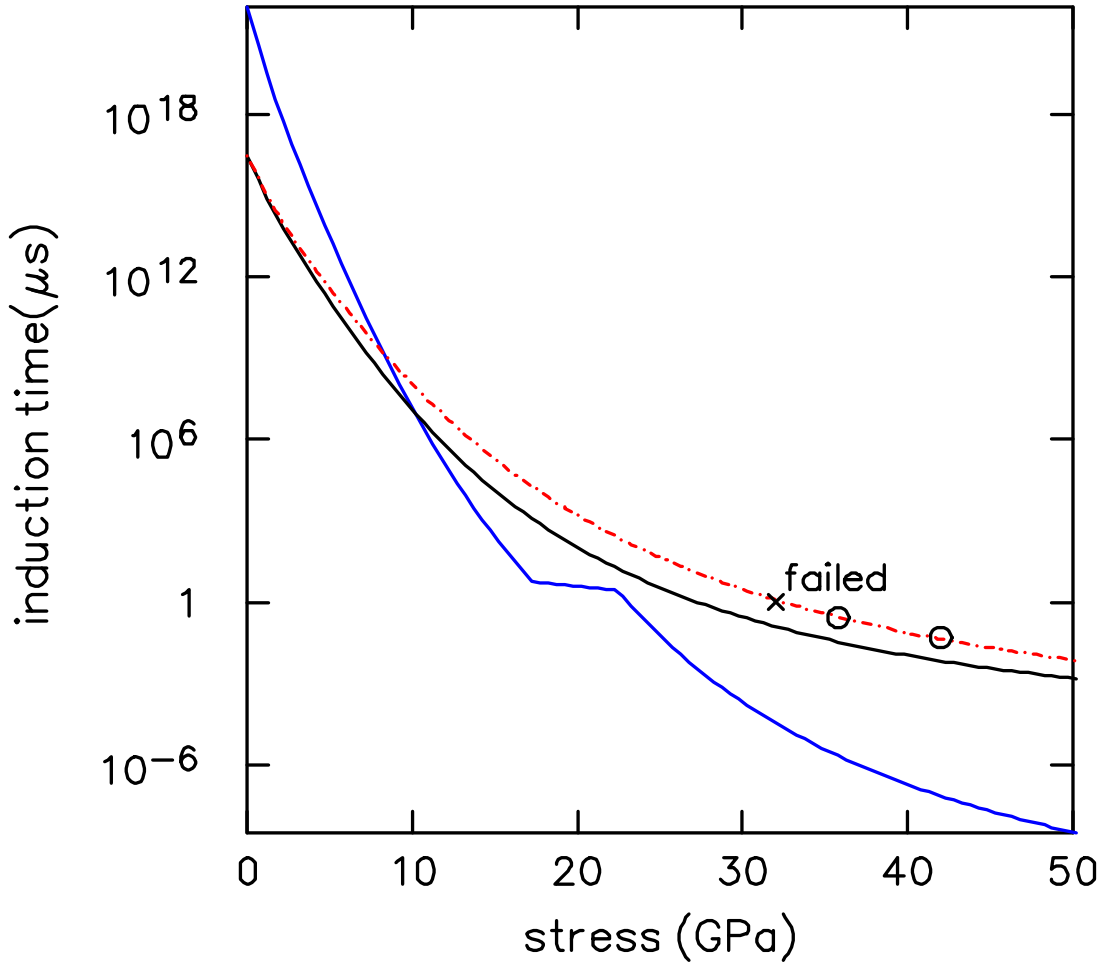
carbon in green, nitrogen in blue,
oxygen in red and hydrogen in grey

PBX-9501 Pop-plot and HMX induction time



Hot spots dominate ignition of PBX

Single crystal HMX initiation



Blue line: liquid Arrhenius reaction rate

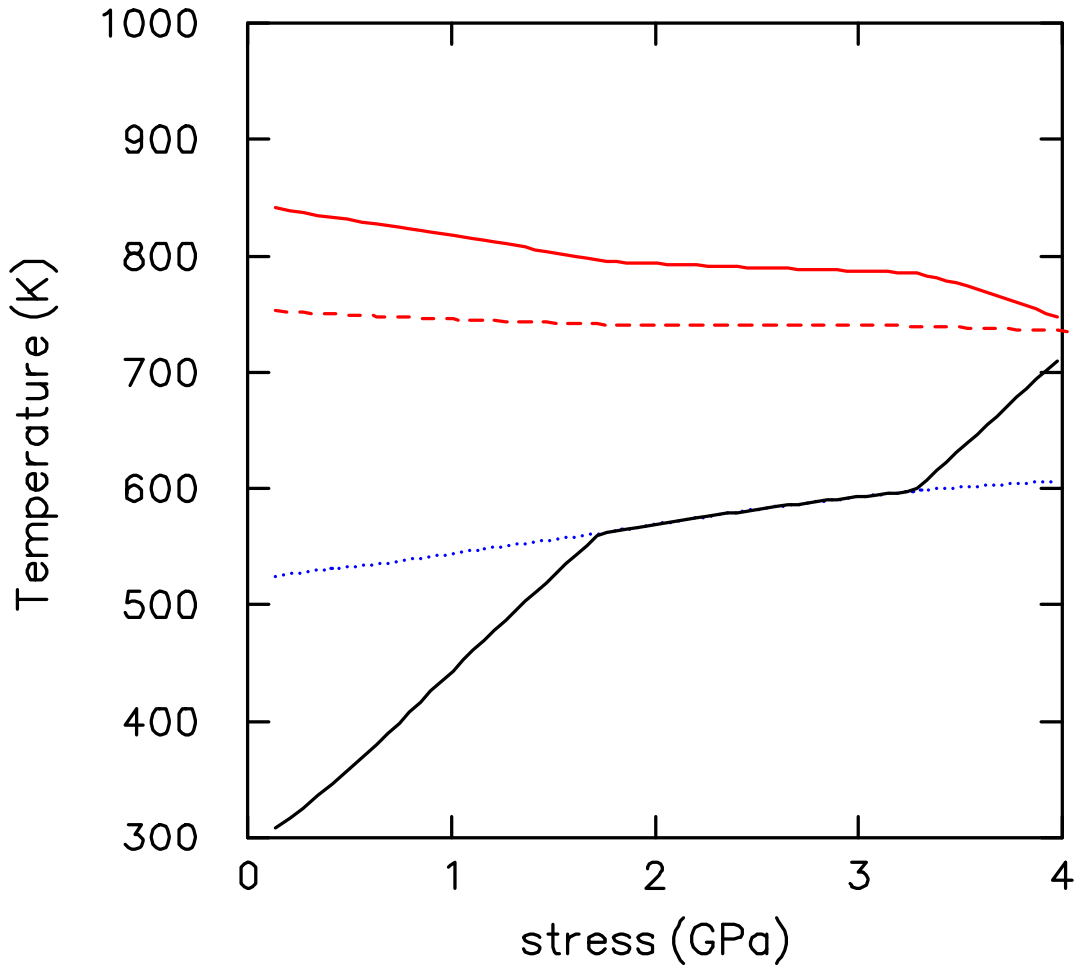
Red and black lines: Solid Arrhenius reaction rate sensitivity to specific heat

Symbols are experiments by Craig
32 GPa failed detonation after 6.6 mm run
CJ pressure is 36 GPa

Single crystal is very insensitive

Hot-Spot temperature for 1 μs induction time

Granular HMX, 35% porosity



Solid red line 1 μm hot spot

Dashed line 10 μm hot spot

Black line is shock temperature

Dotted blue line is liquid-solid coexistence curve

Hot spots above melting

$$\frac{\text{Latent heat}}{C_v} \approx 200 \text{ K}$$

Hot-Spot evolution

1. Temperature sensitive reaction rate
Constant volume burn

$$P_{cv} = 15 \text{ GPa and } T_{cv} = 1800 \text{ K}$$

2. Shock in solid

$$P \sim 8 \text{ GPa, } T \sim 490 \text{ K and } u = 0.8 \text{ mm}/\mu\text{s}$$

Negligible reaction

3. Expansion of reaction products in hot spot

$$\frac{T}{T_{cv}} = \left(\frac{\rho_{cv}}{\rho} \right)^\Gamma = (1 + ut/r_0)^{-3\Gamma}$$

In time of $t = r_0/u$ temperature drops by factor 1/8
either quenches reaction
or leads to deflagration wave on hot spot surface.

Ref. Simulations by Mader

- Fast energy release
- Small hot spots quenched by rapid expansion
- Large hot spots grow by deflagration
- Ignition is collective phenomena of many hot spots

Phenomenological Burn models

- **Forest Fire model** (Chuck Forest)
 Single curve build up principle
 Reactive shock trajectory independent of P_0
 Rate(P) from Pop-plot + reactive Hugoniot
 analog of Chisnell-Whitham rule for shock in duct
 relates change in shock speed to change in area

- **Ignition & Growth model** (Lee & Tarver)

$$\text{Rate}(V, P, \lambda) = \underbrace{I \cdot (1 - \lambda)^x (V_0/V - 1)^r}_{\text{Ignition}} + \underbrace{G \cdot (1 - \lambda)^x \lambda^y P^z}_{\text{Growth}}$$

- **JTF model** (Johnson-Tang-Forest)
 Additional internal degrees of freedom
 Hot-spot mass fraction f and temperature T_s
 shock pressure P_s (based on artificial dissipation)

$$\frac{df}{dt} = \text{Rate}(T_s)$$

$$\frac{dT_s}{dt} = \frac{\Gamma T_s dP}{k dt} - C_p^{-1} \frac{dq}{dt} \quad \text{and} \quad T_s(P_s) \text{ initially}$$

$$\frac{d\lambda}{dt} = \underbrace{\mu \frac{df}{dt}}_{\text{Ignition}} + \underbrace{\left[1 - \lambda - \mu(1 - f)\right] \left(\frac{f - f_0}{1 - f_0}\right) + G(P, P_s)}_{\text{Growth}}$$

Limitations of Current Burn Models

Tacit assumption on hot-spot distribution
Same as experiment used to calibrate model
One-dimensional for simplicity

Problems sensitive to hot-spot distribution

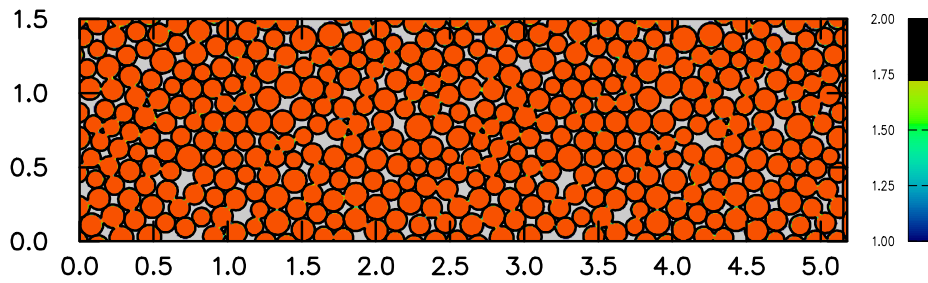
- **Shock desensitization**
Few per cent voids in plastic bonded explosive
Weak shock compress out voids
Reduces heterogeneities
Can extinguish propagating detonation wave
Experiments by Campbell & Travis on PBX-9404
- **Corner turning**
Rarefactions from side
quenches growth of hot spots
partially burnt regions or dead zones
- **Failure diameter**
Also, curvature effect
Hot spots affect propagation of detonation wave
- **Structure of heterogeneous**
Grain size effects
Specific surface area effects growth of hot spots
Pressed vs. cast TNT
Surface area and connectivity of pores
Effect of damage and aging

Granular Explosive

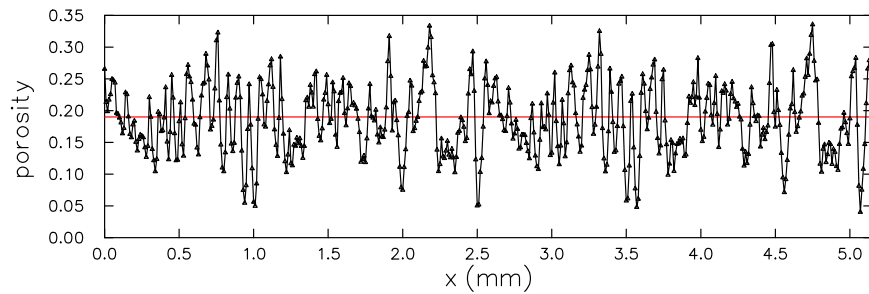
- Model for damaged explosives
Degree of freedom from porosity
- More sensitive to ignition
More heterogeneities than solid
Exacerbates effect of hot spots
Deflagration-to-Detonation Transition experiments
Longer time scale than for shock initiation
Multiple waves more important
- Two-Phase models
Coarse grained thermodynamic variables
Homogenized theory with volume fraction
Hot spots not resolved
Require phenomenological burn model
Reaction rate depends on fluctuations

Piston driven compaction waves

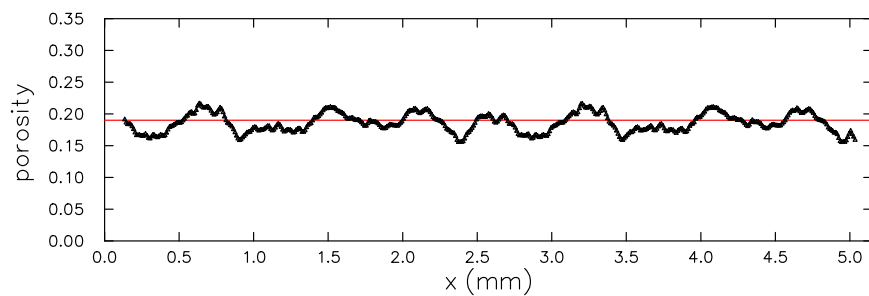
Density (pores are void and shown in gray)



Porosity profile



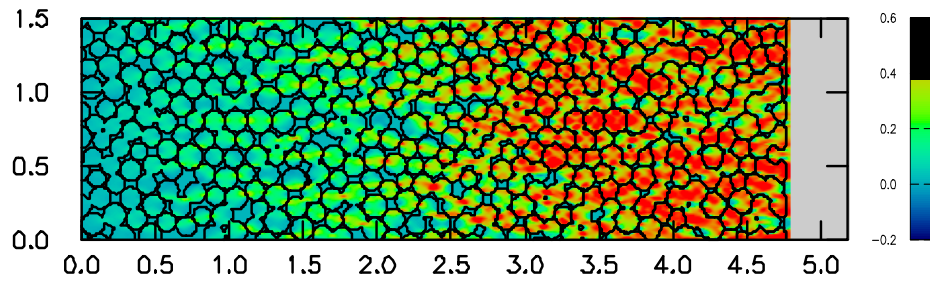
Porosity, smoothed over 2 grain diameters



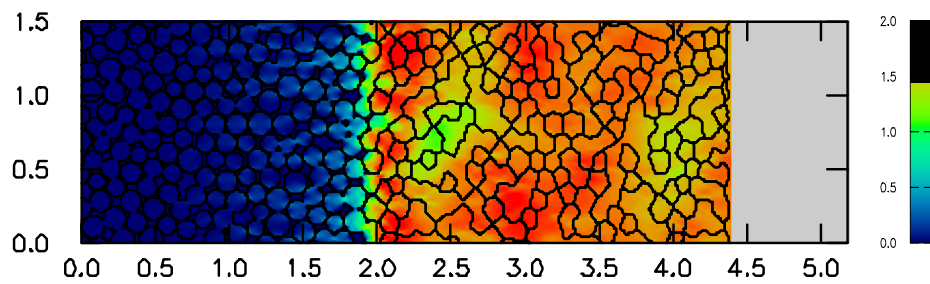
Tightly packed bed HMX grains, 19% porosity

Stress field

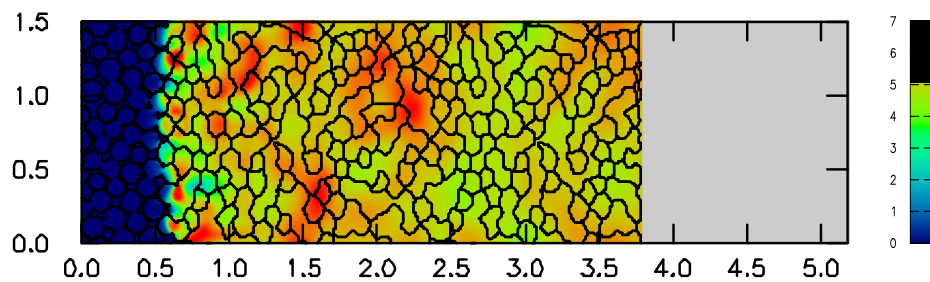
200 m/s piston at time = $2.0 \mu\text{s}$



500 m/s piston at time = $1.6 \mu\text{s}$

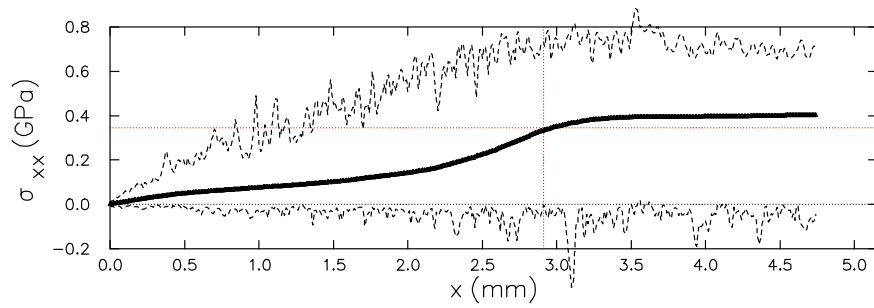


1000 m/s piston at time = $1.4 \mu\text{s}$

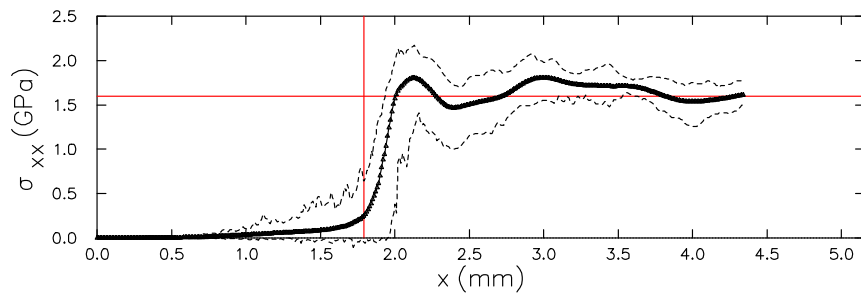


Stress profile

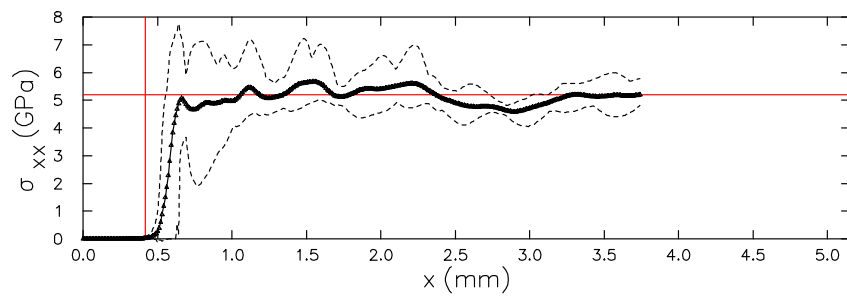
200 m/s piston at time = $2.0 \mu\text{s}$



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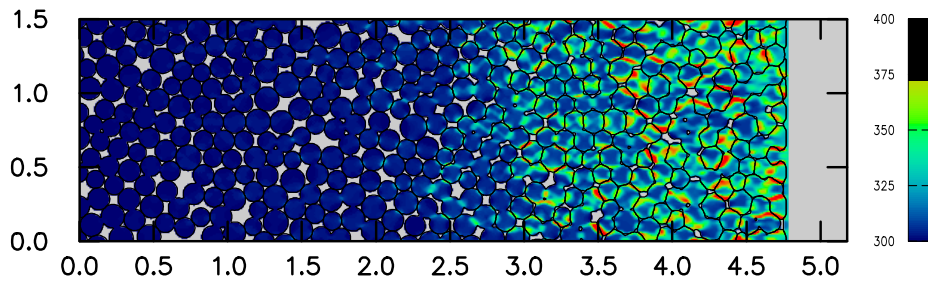


1000 m/s piston at time = $1.4 \mu\text{s}$

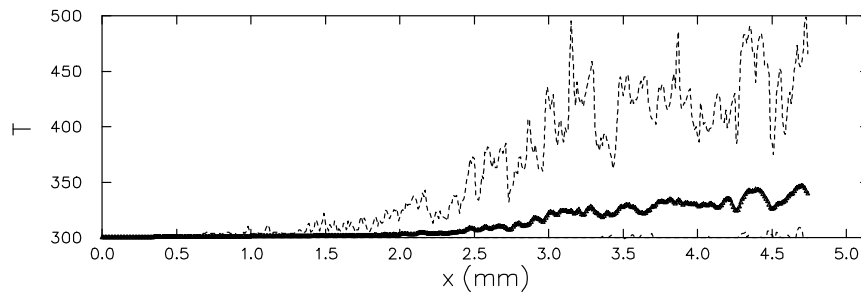


200 m/s piston at time = $2.0 \mu\text{s}$

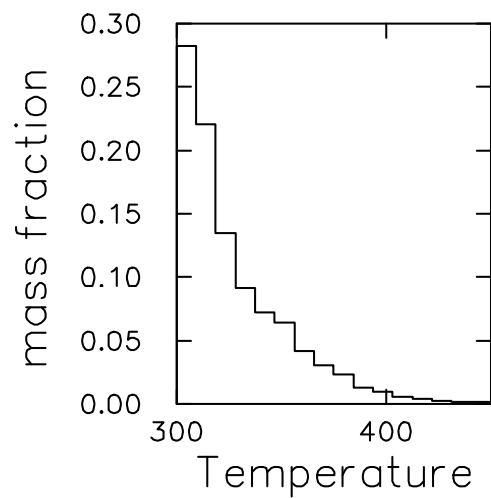
Temperature field



Temperature profile

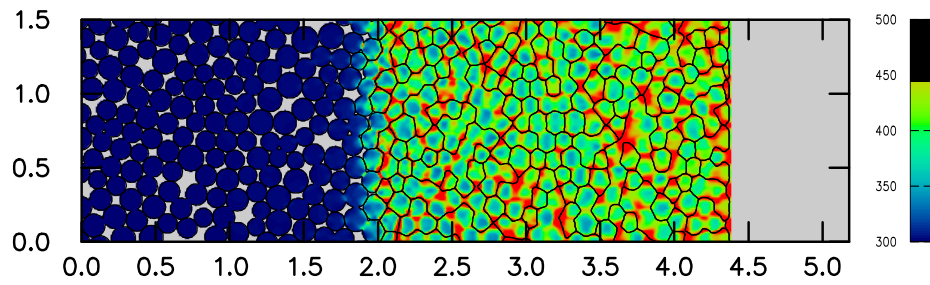


Temperature distribution behind wave

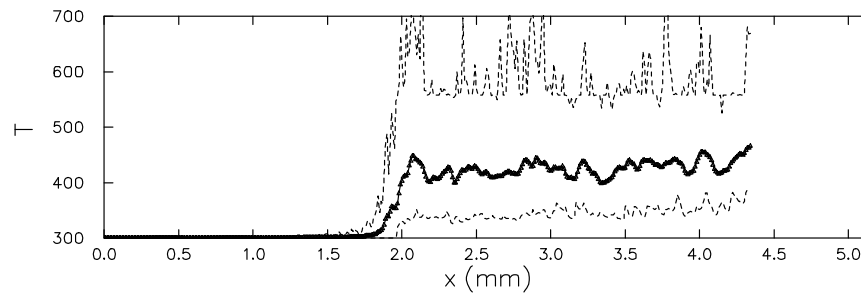


500 m/s piston at time = $1.6 \mu\text{s}$

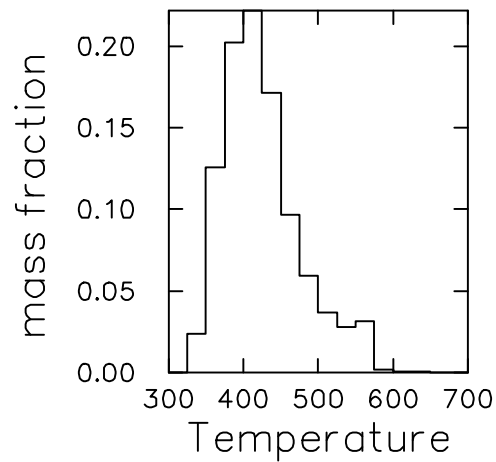
Temperature field



Temperature profile

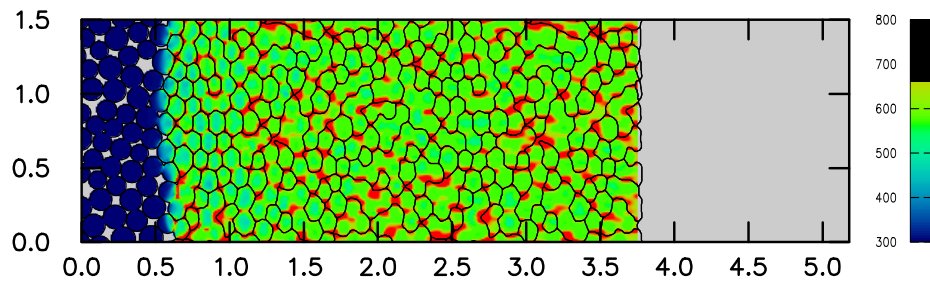


Temperature distribution behind wave

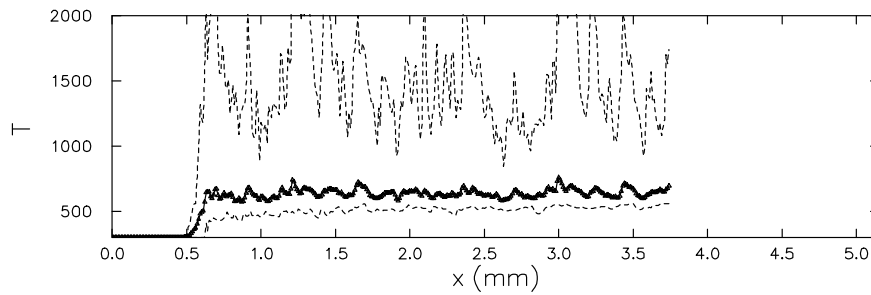


1000 m/s piston at time = $1.4 \mu\text{s}$

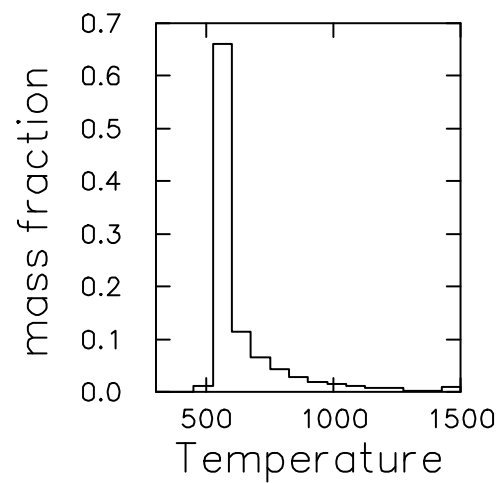
Temperature field



Temperature profile



Temperature distribution behind wave



Improved burn models

Cover wider domain of application

▶ Effect of multiple waves

- Need to incorporate underlying physics

Ignition and growth of hot spots

▶ Insight from meso-scale simulations

Experimental diagnostics do not have resolution

- Ignition stage

Hot spot distribution

Nature of heterogeneities

▶ Internal degrees of freedom

e.g. porosity

Stimuli, strength of wave

Dissipative mechanisms

Plastic work, shear heating, void collapse, etc.

Effect of melting

▶ Governing equations for dynamics

- Growth stage

Hot spots trigger deflagration

▶ Regression rate depends on confinement

▶ Spreading over surface of grains

Gas permeation on grain scale

Connectivity depends on dimension

- Verify model

Velocity profiles from gas gun experiments

Data on average quantities